



US009122289B2

(12) **United States Patent**
Howes

(10) **Patent No.:** **US 9,122,289 B2**
(45) **Date of Patent:** **Sep. 1, 2015**

(54) **CIRCUIT TO CONTROL THE EFFECT OF DIELECTRIC ABSORPTION IN DYNAMIC VOLTAGE SCALING LOW DROPOUT REGULATOR**

(71) Applicant: **Dialog Semiconductor GmbH**,
Kirchheim/Teck-Nabern (DE)

(72) Inventor: **Rupert Howes**, Stroud (GB)

(73) Assignee: **Dialog Semiconductor GmbH**,
Kirchheim/Teck-Nabern (DE)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 392 days.

(21) Appl. No.: **13/692,438**

(22) Filed: **Dec. 3, 2012**

(65) **Prior Publication Data**

US 2014/0152279 A1 Jun. 5, 2014

(51) **Int. Cl.**
H02M 3/157 (2006.01)
G05F 1/10 (2006.01)

(52) **U.S. Cl.**
CPC **G05F 1/10** (2013.01)

(58) **Field of Classification Search**
CPC H02M 3/156; H02M 3/157
USPC 323/273, 274
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,023,097 A 5/1977 Hanashey
4,211,981 A 7/1980 Lerma
5,519,328 A 5/1996 Bennett
5,557,242 A 9/1996 Wetherell

6,294,945 B1 9/2001 Regier et al.
7,816,955 B2 10/2010 Takahashi et al.
8,471,539 B2 * 6/2013 Wu 323/275
8,917,069 B2 * 12/2014 Howes et al. 323/266
2007/0159146 A1 * 7/2007 Mandal 323/280
2011/0181257 A1 * 7/2011 Pancholi et al. 323/280
2012/0299564 A1 11/2012 Howes et al.
2014/0152279 A1 * 6/2014 Howes 323/273

OTHER PUBLICATIONS

"A Wide-Range Logarithmic Charge Digitizer," by A. Richard Zacher, IEEE Transactions on Circuits and Systems—1: Fundamental Theory and Applications, vol. 40, No. 5, May 1993, pp. 307-316.
"500 mA LDO Voltage Regulator," NCP5500, NCV5500, NCP5501, NCV5501, Semiconductor Coponents Industries, LLC, Aug. 2008, pp. 1-13, found <http://onsemi.com>.

* cited by examiner

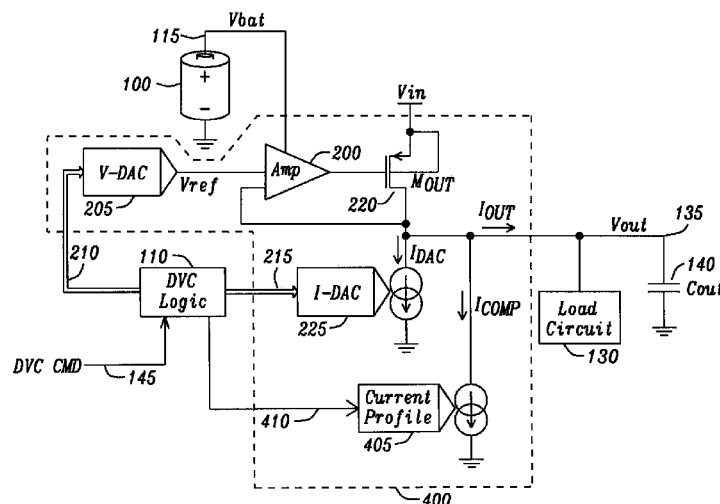
Primary Examiner — Jeffrey Sterrett

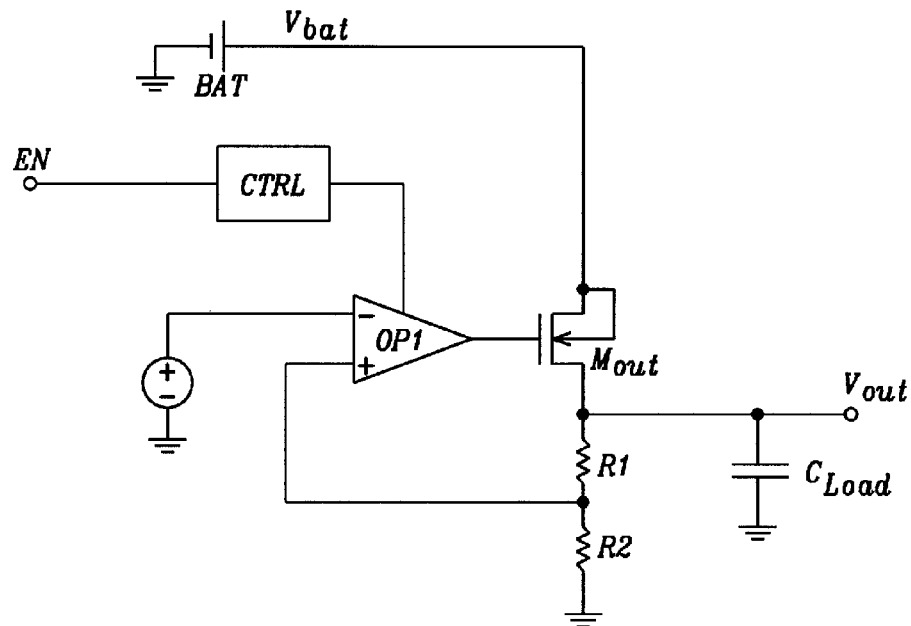
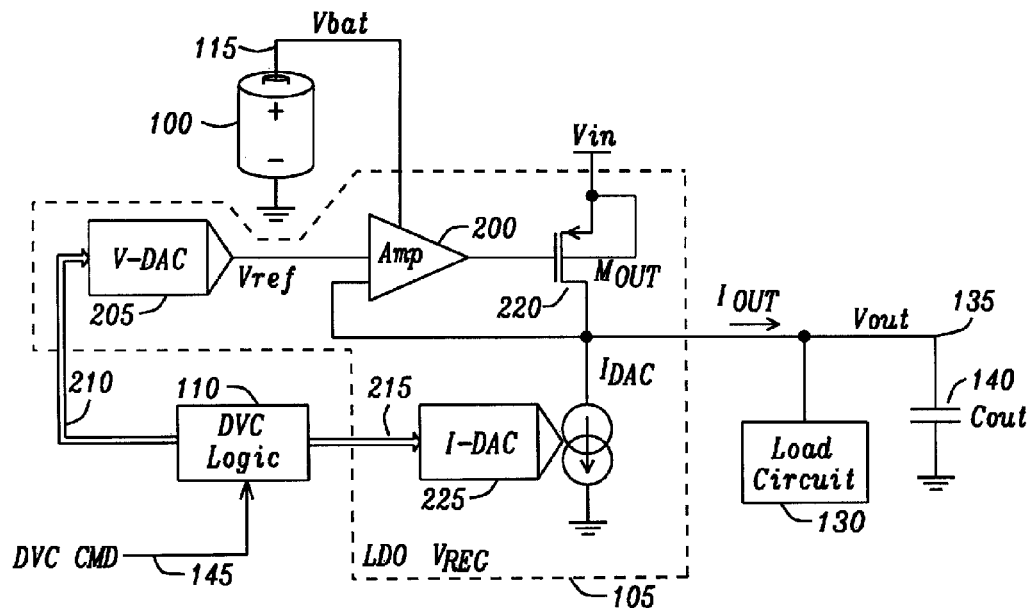
(74) Attorney, Agent, or Firm — Saile Ackerman LLC;
Stephen B. Ackerman; Billy Knowles

(57) **ABSTRACT**

A circuit and method provides compensation for disturbance of an output voltage caused by dielectric absorption of a load capacitor of a low dropout voltage regulator after a modification of the output voltage level of the low dropout voltage regulator. A dielectric absorption current compensation circuit generates a profile current that is applied to an output of the low dropout voltage regulator and in parallel with the load capacitor to compensate for the dielectric absorption current. The dielectric absorption current compensation circuit has a programmable profile current generator that generates the profile current. A switchable current mirror transfers a mirror profile compensation current to the load capacitor to compensate for the dielectric absorption current. In some embodiments, the profile current is a continuous profile dielectric absorption compensation current and in other embodiments, the profile current is a digital profile dielectric absorption compensation current.

22 Claims, 7 Drawing Sheets



*FIG. 1 - Prior Art**FIG. 2*

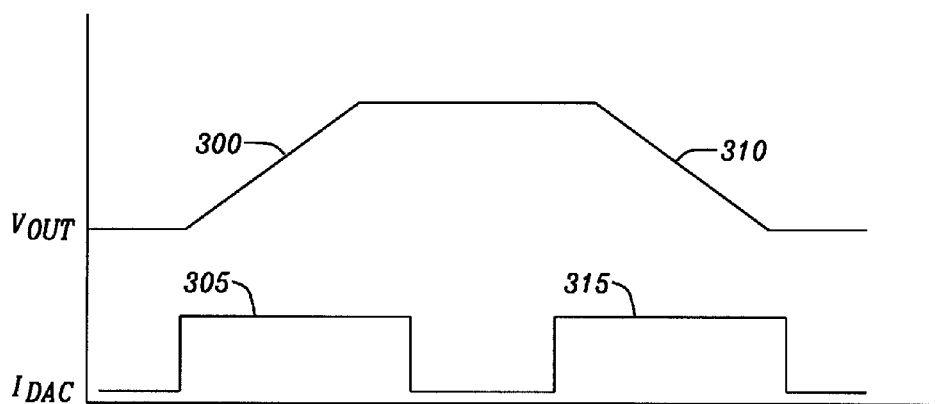


FIG. 3

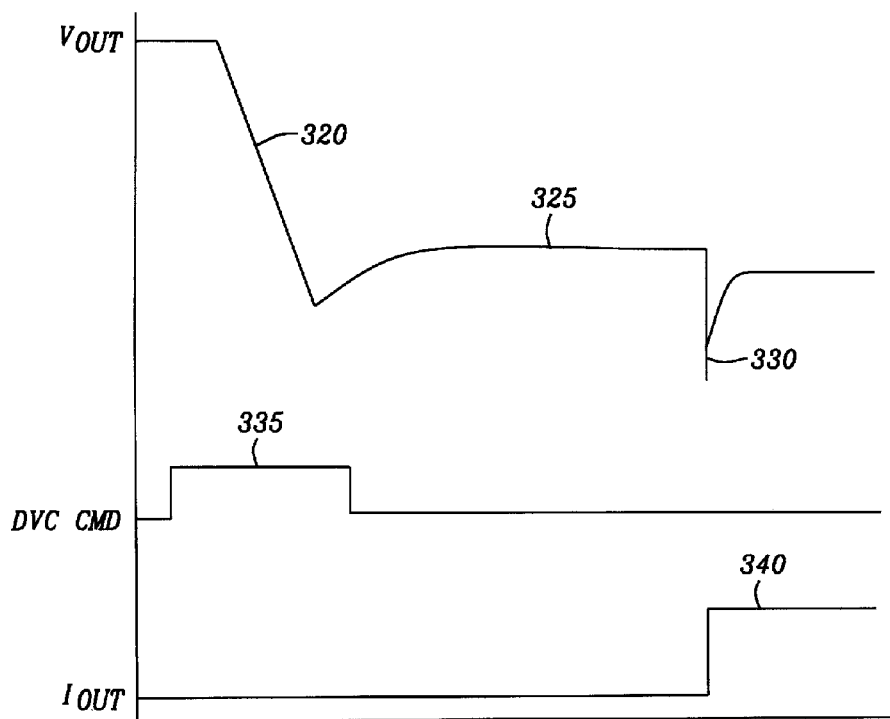


FIG. 4

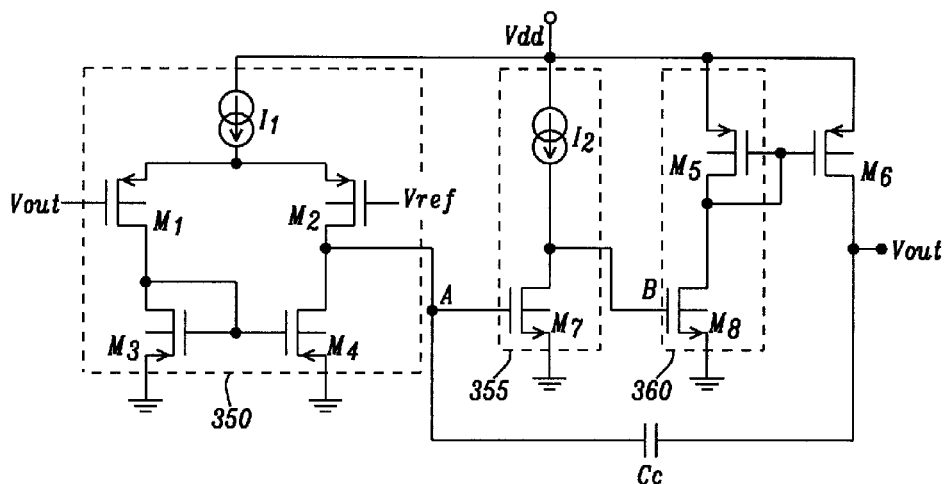


FIG. 5

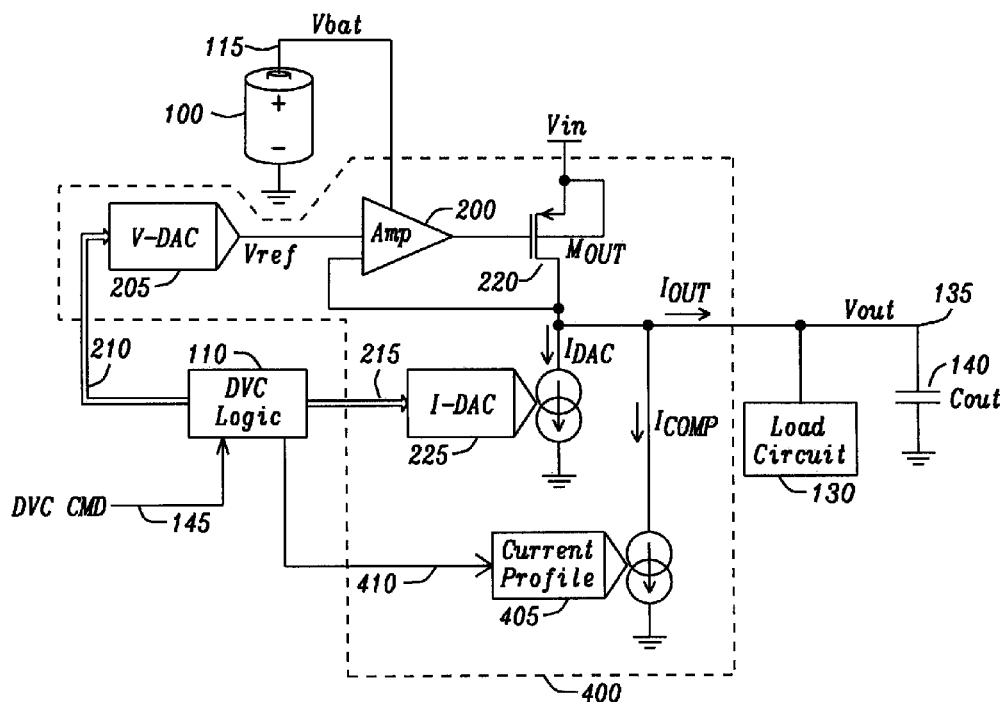


FIG. 6

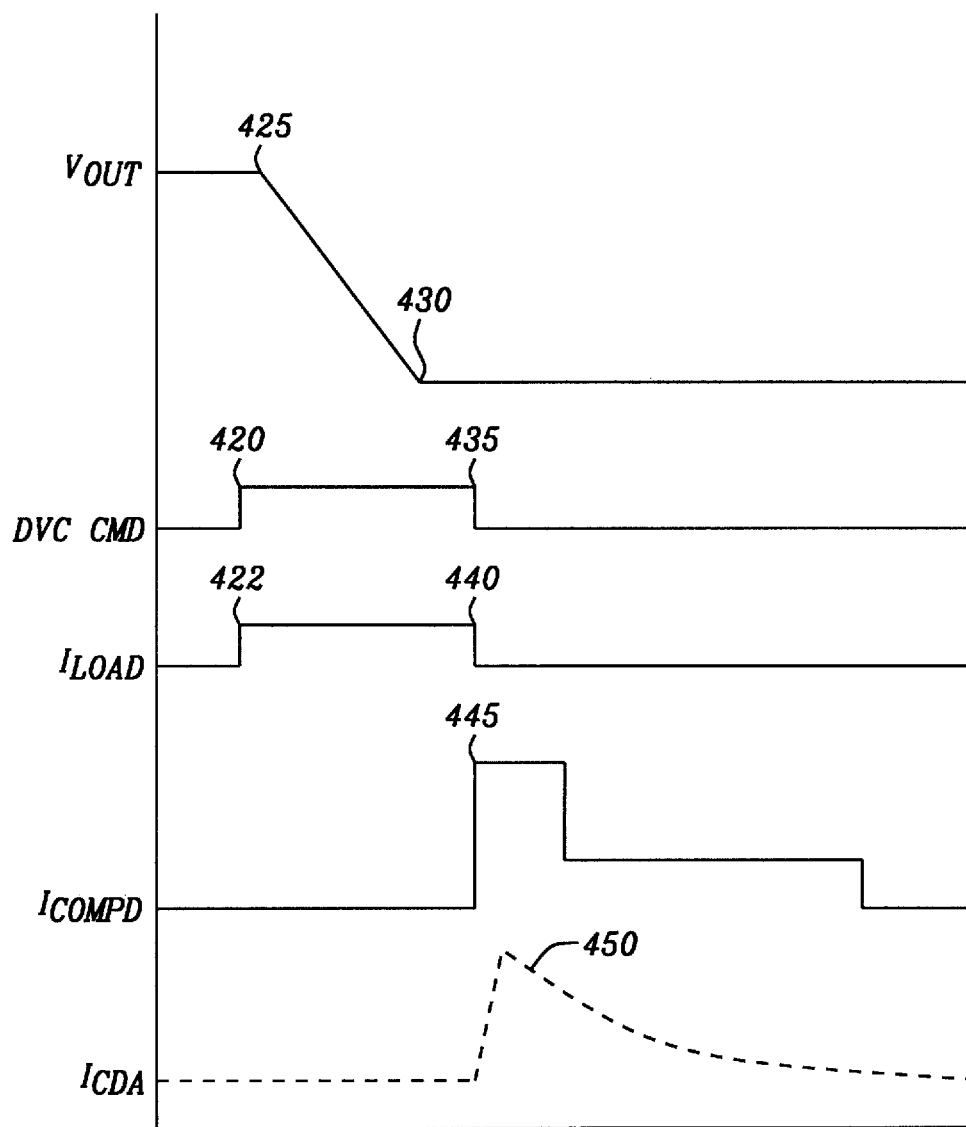


FIG. 7

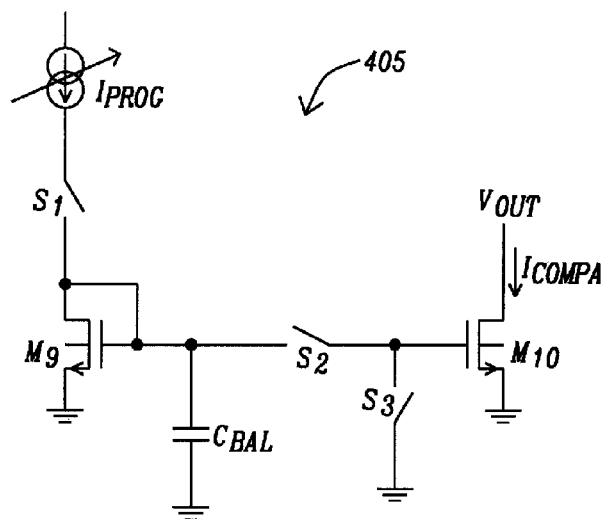


FIG. 8

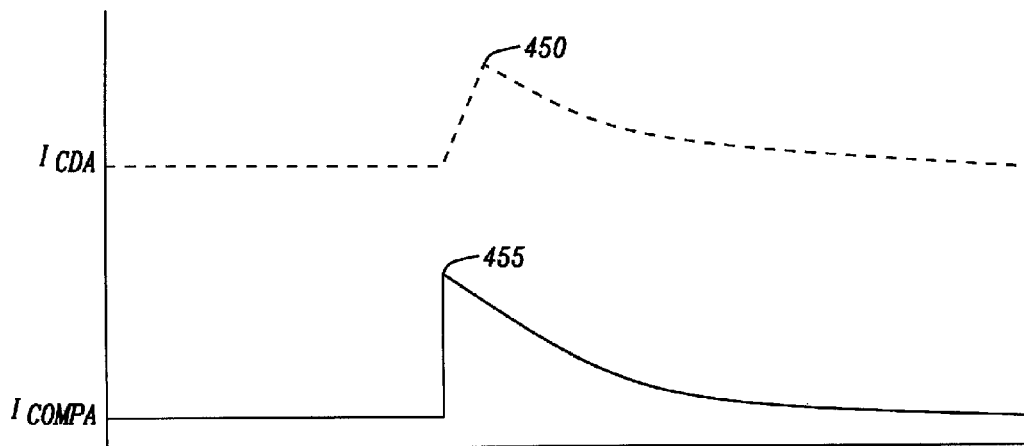


FIG. 9

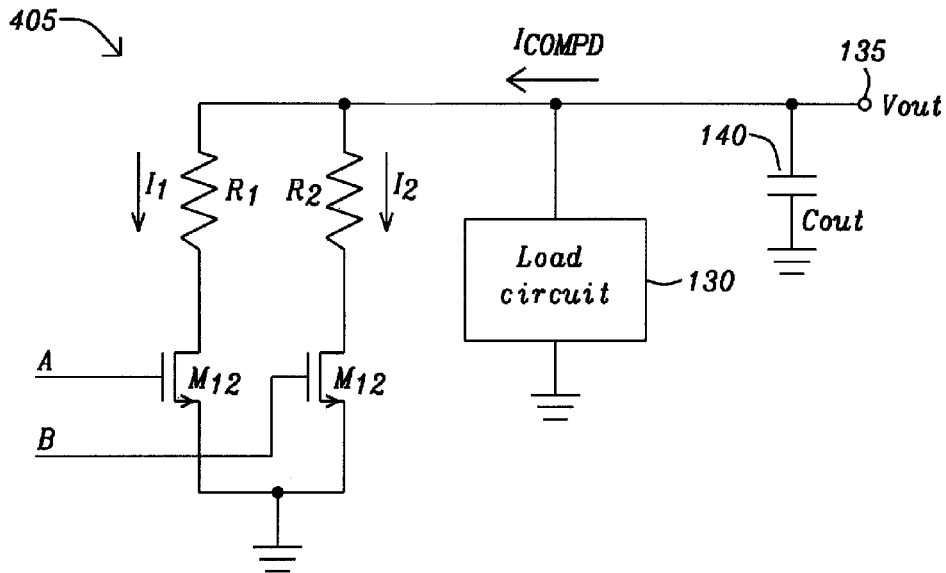


FIG. 10

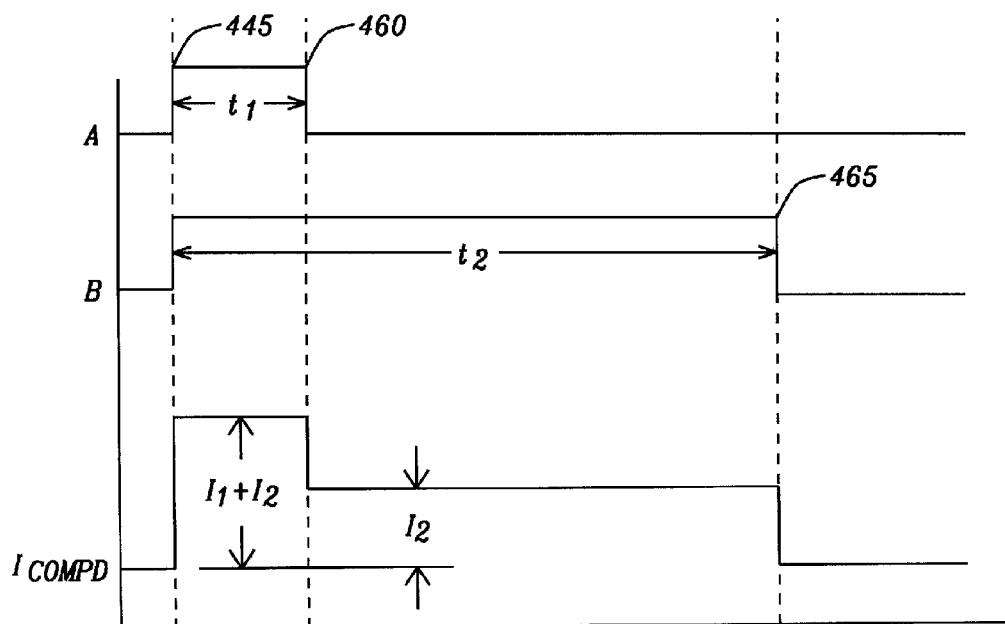
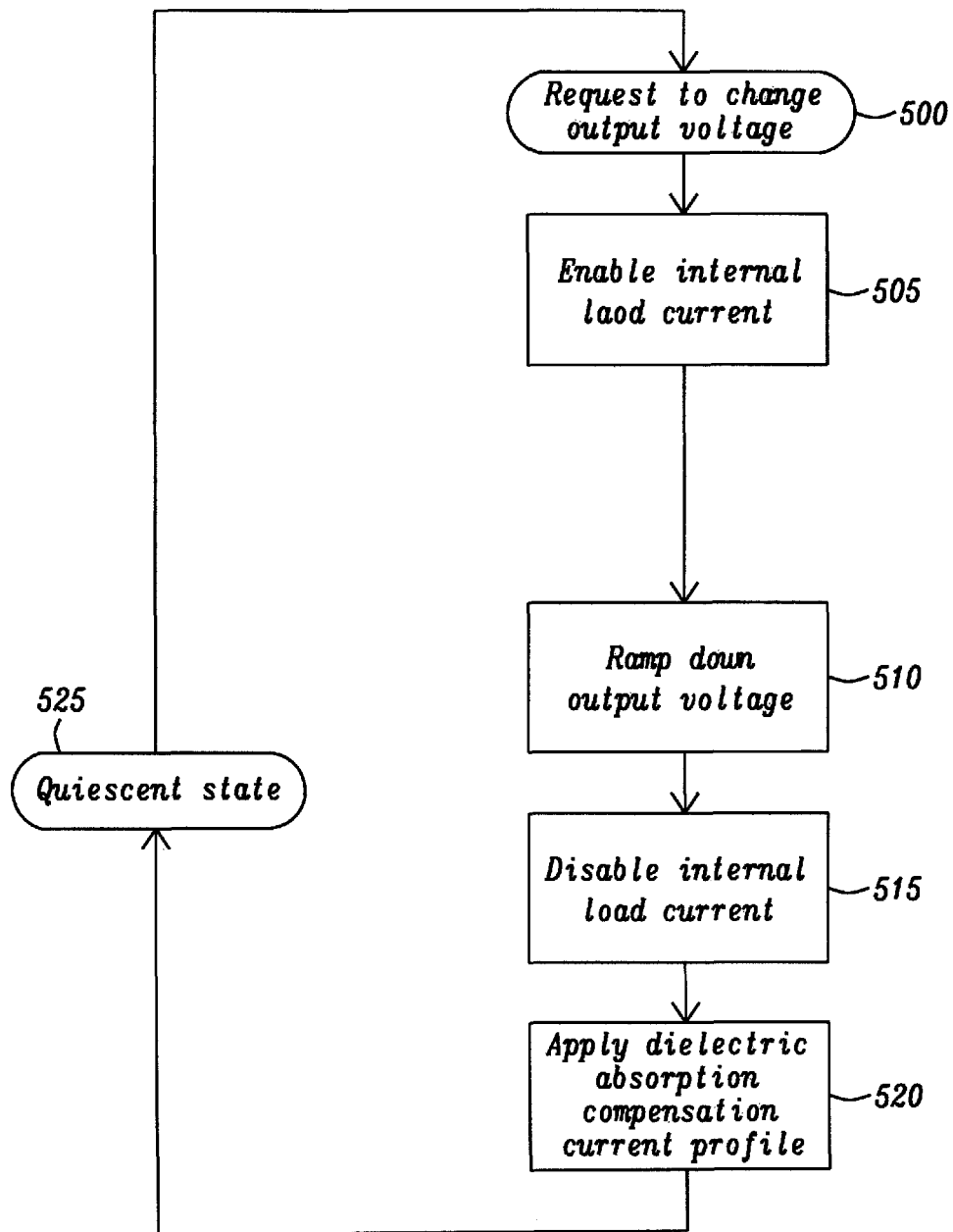


FIG. 11

*FIG. 12*

1

CIRCUIT TO CONTROL THE EFFECT OF DIELECTRIC ABSORPTION IN DYNAMIC VOLTAGE SCALING LOW DROPOUT REGULATOR

RELATED PATENT APPLICATIONS

U.S. patent application Ser. No. 13/134,603 (Howes, et al.), filed on Jun. 10, 2011, assigned to the same assignee as the present invention, and incorporated herein by reference in its entirety.

TECHNICAL FIELD

This disclosure relates generally to voltage regulator circuits. More particularly, this disclosure relates to low dropout voltage regulator circuits. Even more particularly this disclosure relates to circuits and methods for correcting errors due to inherent dielectric absorption of output load capacitors of dynamic voltage control low dropout voltage regulator circuits.

BACKGROUND

Battery powered applications such as smart-phones and tablet computers demand long battery life and therefore highly power efficient circuits. Often, the power supply voltage of digital circuits for the battery power applications must be adjusted during operation to minimize power consumption, since the power dissipated is proportional to the square of the power supply voltage. To achieve the required speed of operation, a certain minimum supply voltage is required. As demand fluctuates, the supply voltage is adjusted as required.

The power supply for these types of circuits is often regulated down from the main battery by a voltage regulator, e.g. buck converter or linear regulator.

Buck voltage converters are generally power efficient but can consume a significant area and need bulky external components (inductors). These circuits are often used for higher load currents where the area of the control circuit is not significant compared with the size of the power switches.

However, for applications that require only a modest load current, the area penalty of a buck converter may be unacceptable. In such cases, the use of a low dropout voltage regulator (LDO) can be more area efficient although with some loss of energy efficiency.

A low dropout regulator is a class of linear regulator that is designed to minimize the saturation of the output pass transistor and its drive requirements. A low-dropout linear regulator will operate with input voltages only slightly higher than the desired output voltage. FIG. 1 is a schematic of a low dropout voltage regulator of the prior art. The main components of a low dropout voltage regulator are a power field effect transistor M_{Out} having a source and bulk connected to a battery BAT to receive a battery voltage V_{bat} . The gate of the power field effect transistor M_{Out} is connected to an output of a differential error amplifier Op1. One input of the differential error amplifier Op1 monitors the fraction of the output determined by the resistor ratio of R1 and R2. The second input to the differential error amplifier Op1 is from a stable voltage reference (bandgap reference) V_{Ref} . If the output voltage rises too high relative to the reference voltage V_{Ref} , the drive to the power field effect transistor M_{Out} changes to maintain a constant output voltage V_{Out} developed across the load capacitance C_{Load} .

Dielectric absorption, also called dielectric relaxation or capacitor soaking, is the tendency of a capacitor to recharge

2

itself after being discharged. Dielectric absorption is also the dominant loss mechanism of the entire usable range of most capacitors that affect the performance of error amplifiers, digital-to-analog converters, other sample and hold circuitry, and switched capacitor circuitry. The load capacitance C_{Load} of the low dropout regulator is a discrete capacitor that is subject to the dielectric absorption phenomena and will impact the functioning of the differential error amplifier Op1 to cause loss of regulation of the low dropout regulator.

SUMMARY

An object of this disclosure is to provide is to provide a circuit and method for compensating for dielectric absorption current of a load capacitor of a low dropout voltage regulator.

To accomplish at least this object, a dielectric absorption current compensation circuit generates a profile current that is applied to an output of the low dropout voltage regulator and in parallel with the load capacitor to compensate for the dielectric absorption current from recharging the load capacitor. In some embodiments, the dielectric absorption current compensation circuit is an analog dielectric absorption current compensation circuit providing an analog profile compensation current mirroring the dielectric absorption current. In other embodiments, digital dielectric absorption current compensation circuit providing a digital profile compensation current having discrete levels approximately mirroring the dielectric absorption current.

The analog dielectric absorption current compensation circuit has a programmable profile current generator that generates the profile current. A switchable current mirror transfers a mirror profile current to the load capacitor to compensate for the dielectric absorption current. The switchable current mirror has a first switch with a first terminal connected to an output of the programmable current source and a second terminal connected to a drain and gate of a diode-connected transistor. A source of the diode-connected transistor is connected to a ground reference voltage source. A ballast timing capacitor has a first plate connected to the drain and gate of the diode-connected transistor and a second plate connected to the ground reference voltage source to control the profile of the compensating current within the dielectric absorption compensation circuit.

A second switch has a first terminal connected to the drain and gate of the diode-connected transistor and second terminal connected to a gate of a second transistor. The drain of the second transistor is connected to an output of the low dropout regulator and in parallel with the output capacitor of the low dropout regulator. A source of the second transistor is connected to the ground reference voltage source. A third switch has a first terminal connected to the gate of the second transistor and the second terminal of the second switch and a second terminal connected to the ground reference voltage source.

When the low dropout regulator is in a steady state condition, the first switch is activated to close the connection from the profile current source to the diode-connected transistor. The second switch is deactivated to disconnect the gate of the second transistor from the drain and gate of the diode-connected transistor. The third switch is activated to connect the gate of the second transistor to the ground reference voltage source.

When the output of the low dropout regulator is programmed to lower voltage level, the output voltage level is brought to the lower voltage level. At this time, the voltage across the output capacitor of the low dropout voltage regulator will begin to recharge and the output voltage will begin

3

to rise. At this time the first switch and the third switch will deactivate and second switch will activate. The analog profile compensation current source will source current with a magnitude that matches the current generated as the output capacitor recharges. The switchable current mirror will provide the mirrored profile current to the output of the low dropout regulator to counteract the current generated by the recharging of the output capacitor.

The digital dielectric absorption current compensation circuit includes a digital-to-analog circuit that receive multiple data bits and generates the digital profile compensation current based on a data state of the data bits. The digital profile compensation current level is generated as the sum of the current levels based on a data state of applied to the data bits. The digital-to-analog circuit has multiple switching transistors that are connected such that a gate of each of the switching transistors receives one of the data bits. The sources of the switching transistors are commonly connected to a ground reference voltage source. A first terminal of each of multiple current determining resistors is connected to a drain of each of the plurality of switching transistors. The second terminals of the current determining resistors are commonly connected to the output of the low dropout voltage regulator for transferring the digital profile compensation current to the load capacitor to compensate for the dielectric absorption current.

When all of the data bits are at a first data state all of the plurality of switching transistors are turned on and the digital profile compensation current is a maximum current level. When all of the data bits are at a second data state all of the plurality of switching transistors are turned off and the digital profile compensation current is a zero current level. When any of the data bits are at a first data state those of the plurality of switching transistors with gates at the first data state are turned on, those of the switching transistors with gates at the second data state are turned off, and the digital profile compensation current is a current level equal to the sum of the current through each of those of the plurality of switching transistors with gates at the first data state and turned on. The digital profile compensation current is formed by selectively setting the data bits to the first data state to approximate the dielectric absorption current.

In some embodiments, at least this object is accomplished by a low dropout voltage regulator including a dielectric absorption current compensation circuit that generates a profile current that is applied to an output of the low dropout voltage regulator and in parallel with the output load capacitor of the low dropout voltage regulator to compensate for the dielectric absorption current of the recharging of the output load capacitor. In some embodiments, the dielectric absorption current compensation circuit is an analog dielectric absorption current compensation circuit providing an analog profile compensation current mirroring the dielectric absorption current. In other embodiments, digital dielectric absorption current compensation circuit providing a digital profile compensation current having discrete levels approximately mirroring the dielectric absorption current.

The analog dielectric absorption current compensation circuit has a profile current generator connected to a switchable current mirror circuit to provide a profile current that mirrors the dielectric absorption recharging current of the output load capacitor of the low dropout regulator. The switchable current generator is deactivated when the low dropout voltage regulator is in a steady state condition (output voltage not changing). It is activated after the low dropout voltage regulator has been programmed to a lower voltage and the output voltage has been reduced. After the output voltage has been reduced, the output load capacitor begins to recharge and the voltage

4

across the output load capacitor begins to rise. To compensate for the recharging voltage, the switchable current source is activated and a mirrored version of the profile current is applied to the output of the low dropout voltage regulator to compensate for the dielectric absorption current of the recharging output load capacitor.

The analog dielectric absorption current compensation circuit has a programmable current source that alters the voltage and therefore the charge stored on a ballast timing capacitor. During normal operation, a first switch is activated to connect the programmable current source to the ballast timing capacitor for charging the ballast timing capacitor to a voltage limited by a diode-connected transistor with the switchable current source. A second switch within the switchable current source is deactivated and a third switch within switchable current source is activated to connect the gate of a second transistor of the switchable current source to the ground reference voltage level to turn off the second transistor. The amount of charge and the voltage level stored on the ballast timing capacitor determines the magnitude of the analog profile compensation current. The higher the voltage level present on the ballast timing capacitor, the greater the analog profile compensation current.

When the analog dielectric absorption current compensation circuit is activated, the first and the third switches are opened and the second switch is closed. The analog compensation current in the second transistor is activated to a current level that is approximately equivalent to the level of the dielectric absorption current caused during the recharging of the output capacitor due to the dielectric absorption. The diode-connected transistor and the second transistor function as a current mirror to provide the analog compensation current to maintain the output voltage level at the output terminal of the low dropout voltage regulator at the disabled voltage level. The ballast timing capacitor is used to control the timing profile for the analog compensation current flowing through the second transistor. When the analog dielectric absorption compensation circuit is activated, the ballast timing capacitor is gradually discharged through the diode-connected transistor. Since the analog compensation current decays over time due to the discharge of ballast timing capacitor through diode-connected transistor, a higher analog compensation current also corresponds to a greater total amount of compensation charge removed from the external capacitor because it takes longer for ballast timing capacitor to be fully discharged.

The digital dielectric absorption current compensation circuit includes a digital-to-analog circuit that receive multiple data bits and generates the digital profile compensation current based on a data state of the data bits. The digital profile compensation current level is generated as the sum of the current levels based on a data state of applied to the data bits. The digital-to-analog circuit has multiple switching transistors that are connected such that a gate of each of the switching transistors receives one of the data bits. The sources of the switching transistors are commonly connected to a ground reference voltage source. A first terminal of each of multiple current determining resistors is connected to a drain of each of the plurality of switching transistors. The second terminals of the current determining resistors are commonly connected to the output of the low dropout voltage regulator for transferring the digital profile compensation current to the load capacitor to compensate for the dielectric absorption current.

When all of the data bits are at a first data state, all of the switching transistors are turned on and the digital profile compensation current is a maximum current level. When all of the data bits are at a second data state all of the plurality of

5

switching transistors are turned off and the digital profile compensation current is a zero current level. When any of the data bits are at a first data state those of the plurality of switching transistors with gates at the first data state are turned on, those of the switching transistors with gates at the second data state are turned off, and the digital profile compensation current is a current level equal to the sum of the current through each of those of the plurality of switching transistors with gates at the first data state and turned on. The digital profile compensation current is formed by selectively setting the data bits to the first data state to approximate the dielectric absorption current.

In some embodiments, at least this object is accomplished by an apparatus performing a method for compensating for the dielectric absorption current from the recharging of the output load capacitor of a low dropout voltage regulator. The low dropout voltage regulator is requested to decrease its output voltage. An internal load current source is enabled to decrease the output voltage of the low dropout voltage regulator by adjusting the charge of the output load capacitor. The output voltage of the low dropout voltage regulator is ramped down until it brought to a lower voltage level and the internal load voltage source is disabled. A profile current is applied after the low dropout voltage regulator is disabled to counteract the dielectric absorption current of the recharging output load capacitor to prevent the low dropout voltage regulator from becoming unregulated.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic of a low dropout voltage regulator of the prior art.

FIG. 2 is a schematic diagram of Howes, et al. of a battery driven power supply including a low dropout voltage regulator with dynamic voltage control.

FIG. 3 is a plot of the timing of the output voltage level of the low dropout voltage regulator and the current of the dynamic voltage control current source of Howes, et al.

FIG. 4 is a plot of the output voltage response of the low dropout voltage regulator after dynamic voltage control current source ramp down with transient load current applied showing excessive transient load response of Howes, et al.

FIG. 5 is a schematic diagram of an error amplifier of the low dropout voltage regulator of FIG. 2.

FIG. 6 is a schematic of an embodiment of a low dropout voltage regulator with dynamic voltage control including a dielectric absorption current compensation circuit of this disclosure.

FIG. 7 is plot of the timing of the low dropout voltage regulator with dynamic voltage control including a dielectric absorption current compensation circuit of this disclosure.

FIG. 8 is a schematic of the dielectric absorption current compensation circuit for implementing continuous time compensation for the capacitor dielectric absorption relaxation current of this disclosure.

FIG. 9 is a plot comparing the continuous time profile current and dielectric absorption relaxation current of the capacitor dielectric absorption compensation circuit of the present disclosure.

FIG. 10 is a schematic of the dielectric absorption current compensation circuit for implementing digital compensation for the capacitor dielectric absorption relaxation current of this disclosure.

FIG. 11 is a plot comparing the digital profile compensation current and dielectric absorption relaxation current of the capacitor dielectric absorption compensation circuit of the present disclosure.

6

FIG. 12 is a flowchart for a method for operating a dynamic voltage controlled low dropout voltage regulator with a capacitor dielectric absorption compensation circuit of the present disclosure.

DETAILED DESCRIPTION

Howes, et al. provides low dropout voltage regulator circuit in which the output voltage can be dynamically increased or decreased in response to a system request. This increase or decrease must be achieved rapidly. The circuit requires no knowledge of the load current. To minimize battery power consumption, the output voltage level of the low-dropout voltage regulation circuit is dynamically adjusted depending on system requirements. To respond to a system request to increase or decrease the output voltage rapidly, which is normally required, the low dropout voltage regulator needs to have a high bandwidth. This requires high power dissipation. In the prior art, a dynamic bias scheme ensures that the quiescent current of the circuit is kept low and only increases when the output voltage is changed (programmed to a new value), which ensures the internal circuit bandwidth (poles) track the output bandwidth (pole). It is apparent that a high circuit bandwidth is achieved only with a high output load current.

In most embodiments of Howes, et al., the low dropout regulator does not require the output load current to be a particular value, but the circuit is forced into a high bandwidth state by applying an internal load current that increases the output pole. The dominant pole of the low dropout regulator is increased via dynamic current sensing. Once this high bandwidth state is reached, changing the reference voltage output from a voltage adjustment circuit such as a voltage digital-to-analog converter ramps the output voltage level up. At the end of the adjusting of the output voltage level, the internal load current may be switched off to save power. The internal load current may be maintained if another adjustment command is expected or a load transient is expected. In other embodiments, the internal load current may be maintained after the end of an adjustment of the output voltage level, but at a lower level. The internal load current for a modification of the output voltage level may be a function of the ramp rate required, the initial ramp voltage, or the end of ramp voltage. In other embodiments, the internal load current may be a function of the load capacitance. In some embodiments, the internal load current could be made a function of the system load current. The system load current is known from dynamic bias sense circuitry.

In various embodiments, the low dropout voltage regulator has a controlled ramp-rate from zero volts to the initial output target voltage during a power initialization by dynamically controlling the voltage adjustment circuit and the internal load current.

FIG. 2 is a schematic diagram of Howes, et al showing a battery 100 driven power supply including a low dropout voltage regulator 105 with dynamic voltage control 110. In the battery-powered systems such as the smart-phone or tablet computer, a power controller provides a power command 145 to indicate the voltage level necessary to be applied to circuitry within the system. During inactivity, many of the circuits within the system are disabled and are activated only during usage. On other occasions, some circuitry has the output voltage level 135 decreased to maintain a minimal performance level. When more performance is demanded the output voltage level 135 is increased to meet the demands of the higher performance. The battery 100 is connected to an amplifier gain stage 200 of the low dropout voltage regulator

7

105 to provide necessary power to the control circuitry of the low dropout voltage regulator 105. The input voltage V_{in} is from a switching voltage regulator that is the voltage applied to the output transistor 220 to generate the output voltage 135 from the low dropout voltage regulator 105. The power command signal 145 is the input to the dynamic voltage control circuit 110. A first output 215 of the dynamic voltage control circuit 110 is connected to adjustable internal load current source 225 of the low dropout voltage regulator 105 to provide a current adjustable internal load current source 225 indicating the voltage level and the rate of change ramping of the output voltage 135. A second output 210 of the dynamic voltage control 110 provides a reference voltage adjustment signal to a voltage digital-to-analog converter 205 to select the reference voltage level V_{ref} for the amplifier 200.

The output voltage 135 is applied to output load capacitor 140 and the output load current source 130. A second input terminal of the first amplifier gain stage 200 is connected to the output terminal of the low dropout voltage regulator 105 to receive a slow feedback signal. The slow feedback signal from the output terminal of the low dropout voltage regulator 105 is compared to the reference voltage V_{ref} supplied by the voltage digital-to-analog converter 205 to the amplifier gain stage 200 to develop a drive signal for the output transistor 220.

In order to rapidly adjust the voltage level V_{out} at the output terminal 135 of the low dropout voltage regulator 105, the internal bandwidth or dominant pole of the low dropout voltage regulator 105 must be increased. To accomplish this and to make the adjustment of the dominant pole independent of the load current 130, an adjustable internal load current source 225 is connected to the output terminal 135 of the low dropout voltage regulator 105. The dynamic voltage control circuit 110 has an output 215 connected to the adjustable internal load current source 225 to provide a current adjustment control signal. The adjustable internal load current source 225 is a current digital-to-analog converter that receives the current adjustment control signal and provides the internal current to the source of the PMOS output transistor 220 to increase the pole of the output of the low dropout voltage regulator 105 and thus to its internal circuitry to allow the rapid adjustment of the output voltage level V_{out} at the output terminal 135.

The internal current output of the adjustable internal load current source 225 is maintained at a level pending another modification of the output voltage level or a transient change in the external load current 130. The load current of the adjustable internal load current source 225 is maintained at a lower level to conserve energy. The load current of the adjustable internal load current source 225 may be in various implementations, a function of the output load capacitance 140. The load current of the adjustable internal load current source 225 may be, in some implementations, a function of a ramp rate of the modification of the output voltage level.

FIG. 3 is a plot of the timing of the output voltage level of the low dropout voltage regulator and the current I_{DAC} of the dynamic voltage control current source 225 of Howes, et al. To minimize the energy consumption from the battery 100, the output voltage level V_{out} of the low dropout voltage regulator 105 is dynamically adjusted depending on system requirements. To respond to the system request 335 to increase 300 or decrease 310 the output voltage level V_{out} at a fast rate the low dropout voltage regulator 105 needs to have a high bandwidth, which in turn requires a large bias current I_{DAC} in the output transistor 220, hence the magnitude of the current I_{DAC} of the adjustable internal load current source 225 is not insignificant. Therefore to keep the efficiency high

8

when the output load circuit 130 is not sinking current, it is desirable to turn off 315 the adjustable internal load current source 225 soon after the end of the ramp down period 310.

FIG. 4 is a plot of the output voltage response of the low dropout voltage regulator 105 after the dynamic voltage control current source 225 ramp down 315 with transient load current I_{OUT} applied showing excessive transient load response of Howes, et al. The output capacitor C_{OUT} is a discrete capacitor that can exhibit varying degrees of dielectric absorption after it has been discharged, where the dielectric continues to relax for some time afterwards. The excess charge can cause the output voltage level V_{OUT} to increase 325 if the load circuit 130 is not sinking any current I_{OUT} . This can cause the low dropout voltage regulator 105 to go out of regulation and the biasing of the error amplifier 200 to become unbalanced. If a transient load is then applied (or a dynamic voltage control circuit 110 ramp up request is received requiring the dynamic voltage control current source 225 load to be applied), the low dropout voltage regulator 105 may be incorrectly biased to be able to respond quickly enough, with the result that the output voltage level V_{OUT} can fall to an unacceptable level 330.

FIG. 5 is a schematic diagram of an error amplifier 225 of the low dropout voltage regulator 105 of FIG. 2. Refer now to FIG. 5 to understand the behavior of the low dropout voltage regulator 105 during the dielectric relaxation period 325 of FIG. 4. The error amplifier 225 of the low dropout voltage regulator 105 of FIG. 2 as shown in FIG. 5 illustrates the first stage 350, the second stage 355, and the third stage or buffer stage 360 that form the error amplifier 225. When the output voltage level V_{out} is forced above the reference voltage V_{ref} , the node A is forced high and node B is forced low shutting off the output transistor 220 completely. If a fast transient load current is now applied, the output voltage level V_{OUT} will fall 325 of FIG. 4 significantly, since node A can only be discharged by the low bias current of the first stage 350 and the dynamic current through the feedback capacitor C_c .

Therefore, what is needed to solve the problem of the capacitor dielectric absorption current is a compensation circuit that will prevent the output voltage level V_{OUT} rising 325 as in FIG. 4 and the node A of FIG. 5 from charging to prevent the output voltage level V_{out} from being forced above the reference voltage V_{ref} . Thus the node A is not forced low and node B is kept high to prevent shutting off the output transistor 220 completely.

FIG. 6 is a schematic of a low dropout voltage regulator 400 with a dynamic voltage control circuit 110 including a dielectric absorption current profile compensation circuit 405. The structure and function of the low dropout voltage regulator 400 with dynamic voltage control circuit 110 is as shown in FIG. 2. The dielectric absorption current profile compensation circuit 405 is connected to the dynamic voltage control circuit 110 to receive an activation signal when the adjustable internal load current source 225 is deactivated to generate a profile current to compensate for the capacitor dielectric absorption current. The output of the dielectric absorption current profile compensation circuit 405 is connected to the output of the low dropout voltage regulator 400 to provide the profile current to compensate for the relaxation current that develops when the output capacitor C_{OUT} recharges resulting from dielectric absorption.

FIG. 7 is plot of the timing of the low dropout voltage regulator 400 with dynamic voltage control 110 including a dielectric absorption current compensation circuit 405 of FIG. 6. A dynamic voltage control command signal 145 changes its state 420 to indicate that the output voltage level 135 is to decrease. The output voltage level V_{OUT} at the output

terminal 135 begins 425 to decrease. The dynamic voltage control logic circuit 110 activates the adjustable internal load current source 225 to maintain 422 the load current I_{LOAD} . When the output voltage level V_{OUT} at the output terminal 135 has decreased to the minimum level 430, the dynamic voltage control command signal 145 changes state 435 again to deactivate the adjustable internal load current source 225 to turnoff 440 the load current I_{LOAD} .

The dielectric absorption current I_{CDA} begins to flow 450 through the output voltage terminal 135 as the output load capacitor 140 begins to recharge because of dielectric absorption. The dielectric absorption current profile compensation circuit 405 is activated 445 to provide a digital profile compensation current I_{COMPD} . In various embodiments, this digital profile compensation current I_{COMPD} has a digital profile that somewhat mirrors the dielectric absorption current I_{CDA} such that when the digital profile compensation current I_{COMPD} is added to the dielectric absorption current I_{CDA} the output voltage level V_{OUT} is held at the new lower level 430 and the error amplifier 200 is not incorrectly activated.

FIG. 8 is a schematic of the dielectric absorption current compensation circuit 405 for implementing continuous time compensation for the capacitor dielectric absorption relaxation for the low dropout voltage regulator of FIG. 6. The dielectric absorption current compensation circuit 405 of FIG. 6 in various embodiments is structured as an analog dielectric absorption current compensation circuit shown in FIG. 8. A programmable current source I_{PROG} is connected to one terminal of a first switch S_1 . A second terminal of the first switch S_1 is connected to the drain and gate of the diode-connected transistor M_9 . The source of the diode-connected transistor M_9 is connected to the ground reference voltage source. The commonly connected drain and gate of the diode-connected transistor M_9 is connected to a first plate of a ballast timing capacitor C_{BAL} . The second plate of the ballast timing capacitor C_{BAL} is connected to the ground reference voltage source. The commonly connected drain and gate of the diode-connected transistor M_9 and the first plate of a ballast timing capacitor C_{BAL} are connected to a first terminal of a second switch S_2 . The second terminal of the second switch S_2 is connected to a gate of a second transistor M_{10} and a first terminal of a third switch S_3 . The second terminal of the third switch S_3 is connected to the ground reference voltage source. The source of the second transistor M_{10} is also connected to the ground reference voltage source. The drain of the second transistor M_{10} is connected to the output terminal 135 of the low dropout voltage regulator.

The programmable current source I_{PROG} alters the voltage and therefore charge stored on the ballast timing capacitor C_{BAL} . During normal operation, the first switch S_1 is activated to connect the programmable current source I_{PROG} to the ballast timing capacitor C_{BAL} to charge the ballast timing capacitor C_{BAL} to a voltage limited by the diode-connected transistor M_9 . The second switch S_2 is deactivated and third switch S_3 is activated to connected the gate of the second transistor M_{10} to the ground reference voltage level to turn off the second transistor M_{10} . The amount of charge and the voltage level stored on the ballast timing capacitor C_{BAL} determines the magnitude of the analog profile compensation current I_{COMPA} . The higher the voltage level present on the ballast timing capacitor C_{BAL} , the greater the analog profile compensation current I_{COMPA} .

FIG. 9 is a plot comparing the continuous time dielectric absorption relaxation current of the capacitor dielectric absorption compensation circuit 405. Referring to FIGS. 8 and 9, at the deactivation of the adjustable internal load current source 225 of FIG. 6, the first and third switches S_1 and S_3

are opened and the switch S_2 is closed. The analog compensation current I_{COMPA} in the second transistor M_{10} is activated to a current level 455 that is approximately equivalent to the level 450 of the dielectric absorption current I_{CDA} caused during the recharging of the output capacitor C_{OUT} due to the dielectric absorption. The diode-connected transistor M_9 and the second transistor M_{10} function as a current mirror to provide the analog compensation current I_{COMPA} to maintain the output voltage level V_{OUT} at the output terminal of the low dropout voltage regulator at the disabled voltage level 430 of FIG. 7. The ballast timing capacitor C_{BAL} is used to control the timing profile for the analog compensation current I_{COMPA} flowing through the second transistor M_{10} . When the capacitor dielectric absorption compensation circuit 405 is activated, the first switch S_1 and the third switch S_3 is deactivated to be opened and the second switch S_2 is activated to be closed. The ballast timing capacitor C_{BAL} is gradually discharged through the diode-connected transistor M_9 . Since the analog compensation current I_{COMPA} decays over time due to the discharge of ballast timing capacitor C_{BAL} through diode-connected transistor M_9 , a higher analog compensation current I_{COMPA} also corresponds to a greater total amount of compensation charge removed from the external capacitor because it takes longer for ballast timing capacitor C_{BAL} to be fully discharged.

In comparison, the digital profile compensation current I_{COMPD} has discrete current levels that start at the higher level 445 and are discretely stepped down in increments to the zero current level. This is opposed to the analog compensation current I_{COMPA} that follows an exponential discharge of the output capacitor C_{OUT} after the recharging due to the dielectric absorption.

FIG. 10 is a schematic of various embodiments of the digital dielectric absorption current compensation circuit 405 for implementing digital compensation of the capacitor dielectric absorption relaxation current of the low dropout voltage regulator of FIG. 6. The embodiment of the digital dielectric absorption current compensation circuit 405 has a first switching transistor M_{11} and a second switching transistor M_{12} . The gate of the first switching transistor M_{11} is connected to receive a first bit A of a logical signal. The drain of the first switching transistor M_{11} is connected to a first terminal of a first current determining resistor R_1 . The gate of the second switching transistor M_{12} is connected to receive a second bit B of the logical signal. The drain of the second switching transistor M_{12} is connected to a first terminal of a second current determining resistor R_2 . The sources of the first switching transistor M_{11} and the second switching transistor M_{12} are commonly connected to the ground reference voltage source. A second terminal of each of the first current determining resistor R_1 and the second current determining resistor R_2 are commonly connected to the output voltage terminal 135 to receive the output voltage level V_{OUT} and the voltage present at a top plate of the output capacitor C_{OUT} and the top terminal of the load circuit 130 connected to the output terminal 135.

FIG. 11 is a plot of the comparing the digital profile compensation current I_{COMPD} and dielectric absorption relaxation current of the capacitor dielectric absorption compensation circuit. Refer now to FIGS. 10 and 11 for a discussion of the operation of the digital embodiment of the dielectric absorption current compensation circuit 405. It should be noted that the structure of the digital embodiment of the dielectric absorption current compensation circuit 405 is essentially the structure of a two-bit digital-to-analog converter. Therefore, the current that is sunk from the output voltage terminal 135 is determined by the output voltage level

11

V_{OUT} , the first current determining resistor R_1 and the second current determining resistor R_2 . The state of the first data bit A and the second data bit B governs the digital dielectric absorption profile current I_{COMP} as the sum of the currents I_1 and I_2 . If first data bit A and the second data bit B are set to a first data state such that the first switching transistor M_{11} and the second switching transistor M_{12} are turned off ($A=B=0$), the digital profile compensation current I_{COMP} is equal to the sum of the currents I_1 and I_2 that have a level of zero.

If the state is of the first data bit A is a first data state to turn on the first switching transistor M_{11} and the second data bit B is a second data state that turns off the second switching transistor M_{12} ($A=1$, $B=0$), the digital profile compensation current I_{COMP} is equal to the current I_1 and the current I_2 has a level of zero. If the state is of the first data bit A is the second data state to turn off the first switching transistor M_{11} and the second data bit B is the first data state that turns on the second switching transistor M_{12} ($A=0$, $B=1$), the digital profile compensation current I_{COMP} is equal to the current I_1 and the current I_2 has a level of zero. If the state is of the first data bit A and the second data bit B is the first data state such that the first switching transistor M_{11} and the second switching transistor M_{12} are turned on ($A=B=1$), the digital profile compensation current I_{COMP} is equal to the sum of the level of the currents I_1 and I_2 .

When the adjustable internal load current source **225** has completed the ramping of the output voltage level V_{OUT} to the lower voltage level, the first and second data bits A and B are set to the first data state such that the first switching transistor M_{11} and the second switching transistor M_{12} are turned on ($A=B=1$) for the time period t_1 . The digital profile compensation current I_{COMP} rises **455** to be equal to the sum of the level of the currents I_1 and I_2 . At the end **460** of the time period t_1 , the first data bit A becomes set to the second data state and the first switching transistor M_{11} is turned off the and the second data bit B remains at the first data state to keep the second switching transistor M_{12} ($A=0$, $B=1$) turned on. The digital profile compensation current I_{COMP} falls at the end **460** of the time period t_1 to be equal to the level of the current I_2 . The second switching transistor M_{12} remains turned on until the end **465** of the time period t_2 . At the end of the end **465** of the time period t_2 , the first data bit A and the second data bit B are set to the first data state such that the first switching transistor M_{11} and the second switching transistor M_{12} are turned off ($A=B=0$) and the digital profile compensation current I_{COMP} brought to a level of zero.

While the current I_1 and the current I_2 are shown to be equal in the embodiments as shown, the current I_1 and the current I_2 in various embodiments may have different levels. Further, in other embodiments, there may be any number data bits with attendant switching transistors and current determining resistors connected as described above. This permits generating a digital profile compensation current I_{COMP} that more nearly simulates a mirror current of the dielectric absorption relaxation current.

FIG. **10** is a flowchart for a method for operating a dynamic voltage controlled low dropout voltage regulator with a capacitor dielectric absorption compensation circuit. An apparatus that performs this method such as the low dropout voltage regulator **400** with a dynamic voltage control circuit **110** including a dielectric absorption current profile compensation circuit **405**, begins by receiving (Box **500**) a request to change the output voltage of the low dropout voltage regulator. The dynamic voltage control circuit **110** activates (Box **505**) the adjustable internal load current source **225** to cause the output voltage level V_{OUT} to decrease (Box **510**). When the output voltage level V_{OUT} has reached it new lower level,

12

the adjustable internal load current source **225** is disabled (Box **515**) and the dielectric absorption current profile compensation circuit **405** is activated (Box **520**) to generate the dielectric absorption profile current I_{COMP} to compensate for the current caused by the recharging of the output capacitor C_{OUT} because of dielectric absorption. When the dielectric absorption has been completed, the dielectric absorption current profile compensation circuit **405** is deactivated and the low dropout voltage regulator assumes (Box **520**) a quiescent state.

While this disclosure has been particularly shown and described with reference to the preferred embodiments thereof, it will be understood by those skilled in the art that various changes in form and details may be made without departing from the spirit and scope of the disclosure.

What is claimed is:

1. A low dropout voltage regulator comprising:

an analog dielectric absorption current compensation circuit providing an analog profile compensation current mirroring the dielectric absorption current that is applied to an output of the low dropout voltage regulator and in parallel with a load capacitor to compensate for the dielectric absorption current comprising:

an analog profile current generator that generates the analog profile compensation current and in communication with the output of the low dropout voltage regulator for transferring the analog profile compensation current to the load capacitor to compensate for the dielectric absorption current;

a first switch with a first terminal connected to an output of the programmable current source and a second terminal;

a diode-connected transistor having a commonly connected drain and gate connected to the second terminal of the first switch;

a ballast timing capacitor having a first plate connected to the drain and gate of the diode-connected transistor and a second plate connected to the ground reference voltage source for controlling the profile of the profile compensation current within the dielectric absorption compensation circuit;

a second switch having a first terminal connected to the commonly connected drain and gate of the diode-connected transistor and second terminal;

a second transistor having a gate connected to the second terminal of the second switch, a drain connected to an output of the low dropout regulator and in parallel with the output capacitor of the low dropout regulator; and

a third switch having a first terminal connected to the gate of the second transistor and the second terminal of the second switch and a second terminal connected to the ground reference voltage source;

wherein when the output of the low dropout regulator is disabled and the output voltage level is placed at a lower voltage level and the voltage across the output capacitor of the low dropout voltage regulator will begin to recharge and the output voltage will begin to rise, the second switch will activate and the first and third switches will deactivate, the ballast timing capacitor will discharge through the diode-connected transistor to cause the second transistor to source the profile compensation current with a magnitude that matches the current generated at the output capacitor recharges to the output of the low dropout regulator to counteract the current generated by the recharging of the output capacitor.

13

2. The low dropout voltage regulator of claim 1 wherein when the low dropout regulator is in a steady state the first switch is activated to close the connection from the profile current source to the diode-connected transistor, the second switch is deactivated to disconnect the gate of the second transistor from the drain and gate of the diode-connected transistor, and the third switch is activated to connect the gate of the second transistor to the ground reference voltage source.

3. An analog dielectric absorption current compensation circuit for generating an analog profile compensation current mirroring the dielectric absorption current that is applied to an output of a low dropout voltage regulator and in parallel with a load capacitor to compensate for the dielectric absorption current comprising:

a profile current generator that generates the analog profile compensation current and in communication with the output of the low dropout voltage regulator for transferring the analog profile compensation current to the load capacitor to compensate for the dielectric absorption current, comprising:

a first switch with a first terminal connected to an output of the programmable current source and a second terminal;

a diode-connected transistor having a commonly connected drain and gate connected to the second terminal of the first switch;

a ballast timing capacitor having a first plate connected to the drain and gate of the diode-connected transistor and a second plate connected to the ground reference voltage source for controlling the profile of the profile compensation current within the dielectric absorption compensation circuit;

a second switch having a first terminal connected to the commonly connected drain and gate of the diode-connected transistor and second terminal;

a second transistor having a gate connected to the second terminal of the second switch, a drain connected to an output of the low dropout regulator and in parallel with the output capacitor of the low dropout regulator; and

a third switch having a first terminal connected to the gate of the second transistor and the second terminal of the second switch and a second terminal connected to the ground reference voltage source;

wherein when the output of the low dropout regulator is disabled and the output voltage level is placed at a lower voltage level and the voltage across the output capacitor of the low dropout voltage regulator will begin to recharge and the output voltage will begin to rise, the second switch will activate and the first and third switches will deactivate, the ballast timing capacitor will discharge through the diode-connected transistor to cause the second transistor to source the profile compensation current with a magnitude that matches the current generated as the output capacitor recharges to the output of the low dropout regulator to counteract the current generated by the recharging of the output capacitor.

4. The dielectric absorption current compensation circuit of claim 3 wherein when the low dropout regulator is at a steady state the first switch is activated to close the connection from the profile current source to the diode-connected transistor, the second switch is deactivated to disconnect the gate of the second transistor from the drain and gate of the diode-

14

connected transistor, and the third switch is activated to connect the gate of the second transistor to the ground reference voltage source.

5. A digital dielectric absorption current compensation circuit for generating a digital profile compensation current mirroring the dielectric absorption current that is applied to an output of a low dropout voltage regulator and in parallel with a load capacitor to compensate for the dielectric absorption current comprising:

a profile current generator that generates the digital profile compensation current and in communication with the output of the low dropout voltage regulator for transferring the digital profile compensation current to the load capacitor to compensate for the dielectric absorption current, comprising:

a digital-to-analog circuit receive a plurality of data bits and generating the digital profile compensation current wherein each data bit represents a current level such that all the current levels are summed together based on a data state of applied to the data bits.

6. The dielectric absorption current compensation circuit of claim 5 wherein the digital-to-analog circuit comprises:

a plurality of switching transistors connected such that a gate of each of the switching transistors received one of the plurality of data bits, the sources of the switching transistors are commonly connected to a ground reference voltage source; and

a plurality of current determining resistors, wherein a drain of each of the plurality of switching transistors is connected to a first terminal of one of the plurality of current determining resistors and second terminals of the current determining resistors are commonly connected to the output of the low dropout voltage regulator for transferring the digital profile compensation current to the load capacitor to compensate for the dielectric absorption current.

7. The dielectric absorption current compensation circuit of claim 6 wherein when all of the data bits are at a first data state all of the plurality of switching transistors are turned on and the digital profile compensation current is a maximum current level.

8. The dielectric absorption current compensation circuit of claim 7 wherein when all of the data bits are at a second data state all of the plurality of switching transistors are turned off and the digital profile compensation current is a zero current level.

9. The dielectric absorption current compensation circuit of claim 8 wherein when any of the data bits are at a first data state those of the plurality of switching transistors with gates at the first data state are turned on, those of the plurality of switching transistors with gates at the second data state are turned off, and the digital profile compensation current is a current level equal to the sum of the current through each of those of the plurality of switching transistors with gates at the first data state and turned on.

10. The dielectric absorption current compensation circuit of claim 8 wherein digital profile compensation current is formed by selectively setting the data bits to the first data state to approximate the dielectric absorption current.

11. The low dropout voltage regulator comprising:

a digital dielectric absorption current compensation circuit for generating a digital profile compensation current mirroring the dielectric absorption current that is applied to an output of a low dropout voltage regulator and in parallel with a load capacitor to compensate for the dielectric absorption current comprising:

15

a profile current generator that generates the digital profile compensation current and in communication with the output of the low dropout voltage regulator for transferring the digital profile compensation current to the load capacitor to compensate for the dielectric absorption current, comprising:

a digital-to-analog circuit receive a plurality of data bits and generating the digital profile compensation current wherein each data bit represents a current level such that all the current levels are summed together based on a data state of applied to the data bits.

12. The low dropout voltage regulator of claim **11** wherein the digital-to-analog circuit comprises:

a plurality of switching transistors connected such that a gate of each of the switching transistors receives one of the plurality of data bits, the sources of the switching transistors are commonly connected to a ground reference voltage source; and

a plurality of current determining resistors, wherein a drain of each of the plurality of switching transistors is connected to a first terminal of one of the plurality of current determining resistors and second terminals of the current determining resistors are commonly connected to the output of the low dropout voltage regulator for transferring the digital profile compensation current to the load capacitor to compensate for the dielectric absorption current.

13. The low dropout voltage regulator of claim **12** wherein when all of the data bits are at a first data state all of the plurality of switching transistors are turned on and the digital profile compensation current is a maximum current level.

14. The low dropout voltage regulator of claim **13** wherein when all of the data bits are at a second data state all of the plurality of switching transistors are turned off and the digital profile compensation current is a zero current level.

15. The low dropout voltage regulator of claim **14** wherein when any of the data bits are at a first data state those of the plurality of switching transistors with gates at the first data state are turned on, those of the plurality of switching transistors with gates at the second data state are turned off, and the digital profile compensation current is a current level equal to the sum of the current through each of those of the plurality of switching transistors with gates at the first data state and turned on.

16. The low dropout voltage regulator of claim **15** wherein digital profile compensation current is formed by selectively setting the data bits to the first data state to approximate the dielectric absorption current.

17. A method for compensating for the dielectric absorption current from the recharging of the output load capacitor of a low dropout voltage regulator comprising the steps of:

requesting the low voltage regulator to decrease its output voltage;

16

enabling an internal load current source to decrease the output voltage of the low dropout voltage regulator by adjusting the charge of the output load capacitor; ramping down an output voltage level of the low dropout voltage regulator until it brought to a lower voltage level; disabling the internal load voltage source; and applying a profile compensation current after the low dropout voltage regulator is disabled to counteract the dielectric absorption current of the recharging output load capacitor to prevent the low dropout voltage regulator from becoming unregulated.

18. The method for compensating for the dielectric absorption current of claim **17** wherein applying the profile compensation current comprises the steps of:

generating a continuous profile compensation current and applying the continuous profile compensation current to the output of the low dropout regulator.

19. The method for compensating for the dielectric absorption current of claim **17** wherein applying the profile compensation current comprises the steps of:

generating a digital profile compensation current and applying the digital profile compensation current to the output of the low dropout regulator.

20. An apparatus for compensating for the dielectric absorption current from the recharging of the output load capacitor of a low dropout voltage regulator comprising:

means for requesting the low voltage regulator to decrease its output voltage;

means for enabling an internal load current source to decrease the output voltage of the low dropout voltage regulator by adjusting the charge of the output load capacitor;

means for ramping down an output voltage level of the low dropout voltage regulator until it brought to a lower voltage level;

means for disabling the internal load voltage source; and

means for applying a profile compensation current after the low dropout voltage regulator is disabled to counteract the dielectric absorption current of the recharging output load capacitor to prevent the low dropout voltage regulator from becoming unregulated.

21. The apparatus for compensating for the dielectric absorption current of claim **20** wherein the means for applying the profile compensation current comprises:

means for generating a continuous profile compensation current and means for applying the continuous profile compensation current to the output of the low dropout regulator.

22. The apparatus for compensating for the dielectric absorption current of claim **20** wherein means for applying a profile compensation current comprises:

means for generating a digital profile compensation current and means for applying the digital profile compensation current to the output of the low dropout regulator.

* * * * *